

Research Article

Dynamical Analysis of Long Fiber-Reinforced Laminated Plates with Elastically Restrained Edges

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This paper presents a variational formulation for the free vibration analysis of unsymmetrically laminated composite plates with elastically restrained edges. The study includes a micromechanics approach that allows starting the study considering each layer as constituted by long unidirectional fibers in a continuous matrix. The Mori-Tanaka method is used to predict the mechanical properties of each lamina as a function of the elastic properties of the components and of the fiber volume fraction. The resulting mechanical properties for each lamina are included in a general Ritz formulation developed to analyze the free vibration response of thick laminated anisotropic plates resting on elastic supports. Comprehensive numerical examples are computed to validate the present method, and the effects of the different mechanical and geometrical parameters on the dynamical behavior of different laminated plates are shown. New results for general unsymmetrical laminates with elastically restrained edges are also presented. The analytical approximate solution obtained in this paper can also be useful as a basis to deal with optimization problems under, for instance, frequency constraints.

1. Introduction

Fiber-reinforced composite laminated plates are extensively used in many engineering applications. The free vibration analysis of these plates plays a very important role in the design of civil, aerospace, mechanical, and marine structures. In addition to the favorable high specific strength and high specific stiffness, fiber-reinforced composite laminates offer the possibility of optimal design through the variation of stacking pattern, angle of fiber orientation, fiber content, and so forth, known as composite tailoring. All these mechanical and geometrical characteristics, as well as the various coupling effects that take place, must be considered in the prediction of the laminates dynamical response to assure that this is reliable, accurate, and adequate to the design requirements.

It is well known that laminated composite plates have relatively low transverse shear stiffness, playing the shear deformation an important role in the global and local behavior of these structures. Among the numerous theories used for laminated plates that include the transverse shear strain,

the first-order shear deformation theory (FSDT) [1, 2] is adequate for the computation of global responses (such as natural frequencies) and simultaneously has some advantages due to its simplicity and low computational cost. Many investigations have been reported for free vibration analysis of moderately thick composite laminates using the FSDT kinematics (see for instance [3–13]). However, the results are, in most cases, limited to certain lamination schemes and boundary conditions. As far as the study of thick plates with elastically restrained edges is concerned, most of the previous works are limited to isotropic ones ([14–19] among others). But, limited information is found for the case of thick anisotropic laminated plates resting on elastic supports. For instance, Setoodeh and Karami [20] implemented a layer-wise laminated plate theory linked with three-dimensional elasticity approach for vibration and buckling of symmetric and antisymmetric fiber-reinforced composite plates having elastically restraint edges support and results for cross-ply laminates are presented, whereas Karami et al. [21] applied the differential quadrature method for the free vibration

analysis of moderately thick symmetric laminated plates with elastically restrained edges. For the same boundary conditions, semianalytical solutions for the free vibration of angle-ply symmetrically laminated plates were presented by Ashour [22]. Nallim and Grossi [23] also studied the vibration of symmetric laminated plates resting on elastic support employing the Ritz method and beam orthogonal polynomials as approximated functions. These kind of approximate functions (in one or two variables) have been used by many authors to the free vibration analysis of, both homogeneous and nonhomogeneous, plates (Chakraverty et al. [24–26] and Chow et al. [27], among others).

In this paper, a general Ritz formulation for the free vibration analysis of anisotropic laminated plates is developed. All kind of boundary conditions including elastically restrained edges are considered enhancing the study. This feature allows a more realistic analysis of some structural problems. The analysis includes a micromechanical approach (according to the classification of Altenbach et al. [28]), where the average mechanical properties of each anisotropic lamina are estimated from the known characteristics of the fibers and the matrix materials taking into account the fiber volume ratio and the fiber-packing arrangement. At structural level, the dynamic response of the unsymmetrical laminated plate, with elastically restrained edges, is analyzed using the first-order shear deformation theory and the Ritz method with beam orthogonal polynomials as coordinate functions. The approximate analytical solution developed here is very useful to understand, both qualitatively and quantitatively, the behavior of complex laminated plates.

2. Formulation

2.1. Effective Elastic Moduli of Long Fiber-Reinforced Laminae.

The micromechanics-based Mori-Tanaka method [29] is used in this section to predict the elastic mechanical properties of the orthotropic unidirectional laminae. This method may be viewed as the simplest mean field approach for inhomogeneous materials that encompass the full physical range of phase volume fraction.

Eshelby's results [33] show that if an elastic homogeneous ellipsoidal inclusion in an infinite linear elastic matrix is subjected to an eigenstrain ϵ^T , uniform strain states ϵ^C is induced, and it is related to the eigenstrain by the expression

$$\epsilon^C = \mathbf{S}^E : \epsilon^T, \quad (1)$$

where \mathbf{S}^E is the Eshelby tensor, which depends on the reinforcement dimensions and the Poisson ratio of the matrix ν_m . The components of this tensor for a circular, cylindrical inclusion with an infinite length-to-diameter ratio parallel to the 1-axis (parallel to the fiber direction, Figure 1) are

$$\begin{aligned} S_{1111} = S_{1133} = S_{1122} = 0, \quad S_{3333} = S_{2222} &= \frac{5 - 4\nu_m}{8(1 - \nu_m)}, \\ S_{3322} = S_{2233} &= \frac{4\nu_m - 1}{8(1 - \nu_m)}, \quad S_{3311} = S_{2211} = \frac{\nu_m}{2(1 - \nu_m)}, \\ S_{3232} &= \frac{3 - 4\nu_m}{8(1 - \nu_m)}, \quad S_{1313} = S_{1212} = \frac{1}{4}. \end{aligned} \quad (2)$$

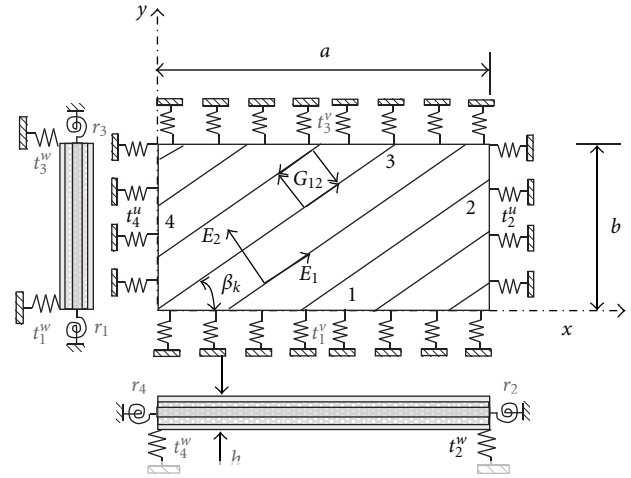


FIGURE 1: General laminated plate resting on elastic supports.

The transformations strains are obtained considering the equivalent homogeneous inclusion for inhomogeneous inclusions developed by Eshelby [33] together with the interaction effects of Mori-Tanaka [29]. These transformations strains are used to equate the total stresses in the inhomogeneities and their equivalent inclusions, as described in the following equation:

$$\mathbf{C}_f : (\epsilon^a + \epsilon^{\text{int}} + \epsilon^C) = \mathbf{C}_m : (\epsilon^a + \epsilon^{\text{int}} + \epsilon^C - \epsilon^T), \quad (3)$$

where \mathbf{C}_f and \mathbf{C}_m are the stiffness tensors of fiber and matrix, respectively, ϵ^a is the uniform far field strain applied to the domain at infinity, and ϵ^{int} is the average elastic strain defined by Mori-Tanaka which is given by

$$\epsilon^{\text{int}} = -k_f (\epsilon^C - \epsilon^T), \quad (4)$$

where k_f is the fiber volume fraction.

Finally, the stiffness tensor \mathbf{C} for different unidirectional laminae can be obtained from energy considerations [34] and (1) to (4) as

$$\begin{aligned} \mathbf{C} = \mathbf{C}_m \times \left\{ \mathbf{I} - k_f \left[(\mathbf{C}_f - \mathbf{C}_m) (\mathbf{S}^E - k_f (\mathbf{S}^E - \mathbf{I}) + \mathbf{C}_m) \right]^{-1} \right. \\ \left. \times (\mathbf{C}_f - \mathbf{C}_m) \right\}^{-1}, \end{aligned} \quad (5)$$

where \mathbf{I} is the fourth order identity tensor.

Using this method the mechanical properties of unidirectional carbon/epoxy laminae are found considering various fiber volume fractions, and they are depicted in Table 1. These properties, for each unidirectional lamina, are then used in the next section to obtain the reduced constitutive matrix.

2.2. General Laminated Plate Resting on Elastic Supports.

Let us consider a rectangular fiber-reinforced composite laminated plate, of dimension $a \times b$ and total thickness h

TABLE 1: Mechanical properties of unidirectional laminae (AS4-3501-6), obtained using Mori-Tanaka method. Fiber and matrix properties $E_{f1} = 225$ GPa, $E_{f2} = 15$ GPa, $G_{f12} = 15$ GPa, $G_{f23} = 7$ GPa, $\nu_{f12} = 0.20$; $E_m = 4.2$ GPa, $\nu_m = 0.34$ ([30]).

k_f	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8
E_1	26.29	48.38	70.46	92.54	114.62	136.70	158.78	180.86
E_2	5.11	5.69	6.31	7.01	7.81	8.76	9.87	11.23
$G_{12} = G_{13}$	1.84	2.17	2.57	3.07	3.70	4.54	5.68	7.35
G_{23}	1.75	1.97	2.22	2.52	2.88	3.32	3.88	4.61
ν_{12}	0.32	0.31	0.29	0.28	0.27	0.25	0.24	0.23

($h = \sum h_k$, h_k represents the thickness of a layer). The laminated plate is composed of an arbitrary number of N_c orthotropic layers and fibre orientation β_k ($k = 1, 2, \dots, N_c$) as shown in Figure 1. A rectangular Cartesian coordinate system (x, y, z) is used to represent the plate geometry and the strain-displacement relations. The x - y plane coincides with the middle plane of the plate. The displacement field of the first-order shear deformation theory is assumed to be of the form [1, 2]

$$\begin{aligned} u(x, y, z, t) &= u_0(x, y, t) + z\phi_x(x, y, t), \\ v(x, y, z, t) &= v_0(x, y, t) + z\phi_y(x, y, t), \\ w(x, y, z, t) &= w_0(x, y, t), \end{aligned} \quad (6)$$

where t is the time dimension u_0, v_0 and w_0 denote the mid-surface translational displacements along the x, y , and z axes, and ϕ_x, ϕ_y are the rotations about y - and x -axes, respectively. The displacement model (6) yields the following kinematic relations:

$$\{\varepsilon\} = \begin{bmatrix} \{\varepsilon_0\} \\ \{\varepsilon_0^*\} \end{bmatrix} + z \begin{bmatrix} \{\varepsilon_1\} \\ \{0\} \end{bmatrix}, \quad (7)$$

where

$$\begin{aligned} \{\varepsilon\}^T &= \{\varepsilon_x, \varepsilon_y, \gamma_{xy}, \gamma_{yz}, \gamma_{xz}\}, \\ \{\varepsilon_0\}^T &= \left\{ \frac{\partial u_0}{\partial x}, \frac{\partial v_0}{\partial y}, \frac{\partial u_0}{\partial y} + \frac{\partial v_0}{\partial x} \right\}, \\ \{\varepsilon_0^*\}^T &= \left\{ \frac{\partial w_0}{\partial y} + \phi_y, \frac{\partial w_0}{\partial x} + \phi_x \right\}, \\ \{\varepsilon_1\}^T &= \left\{ \frac{\partial \phi_x}{\partial x}, \frac{\partial \phi_y}{\partial y}, \frac{\partial \phi_x}{\partial y} + \frac{\partial \phi_y}{\partial x} \right\}. \end{aligned} \quad (8)$$

The stress-strain relation of each layer is given by the generalized Hooke's law as follows:

$$\begin{pmatrix} \sigma_x \\ \sigma_y \\ \tau_{xy} \\ \tau_{yz} \\ \tau_{xz} \end{pmatrix}^{(k)} = \begin{bmatrix} \bar{Q}_{11} & \bar{Q}_{12} & \bar{Q}_{16} & 0 & 0 \\ \bar{Q}_{12} & \bar{Q}_{22} & \bar{Q}_{26} & 0 & 0 \\ \bar{Q}_{16} & \bar{Q}_{26} & \bar{Q}_{66} & 0 & 0 \\ 0 & 0 & 0 & \bar{Q}_{44} & \bar{Q}_{45} \\ 0 & 0 & 0 & \bar{Q}_{45} & \bar{Q}_{55} \end{bmatrix}^{(k)} \begin{pmatrix} \varepsilon_x \\ \varepsilon_y \\ \gamma_{xy} \\ \gamma_{yz} \\ \gamma_{xz} \end{pmatrix}, \quad (9)$$

where \bar{Q}_{ij} are the components of the plane-stress reduced constitutive matrix [35] which are function of the elastic constant determined in Section 2.1 and the ply angle β_k .

2.3. Energy Functional Components. Taking into account (7) and (9), the strain energy due to the laminated plate deflection can be written as

$$U_p = \frac{1}{2} \iint_R \left[\{\varepsilon_0\} [A] \{\varepsilon_0\}^T + \{\varepsilon_0\} [B] \{\varepsilon_1\}^T + \{\varepsilon_1\} [B] \{\varepsilon_0\}^T + \{\varepsilon_1\} [D] \{\varepsilon_1\}^T + \{\varepsilon_0^*\} [A^*] \{\varepsilon_0^*\}^T \right] dx dy, \quad (10)$$

where R is the mid-surface area (Figure 1) and the stiffness coefficients [35, 36] are given by $(A_{ij}, B_{ij}, D_{ij}) = \int_{-h/2}^{h/2} \bar{Q}_{ij}(1, z, z^2) dz$ ($i, j = 1, 2, 6$), $A_{ij}^* = \int_{-h/2}^{h/2} k_{ij} \bar{Q}_{ij} dz$ ($i, j = 4, 5$) k_{ij} being the shear correction factors.

The strain energy corresponding to the elastic edge restraints is given by

$$\begin{aligned} U_t = \frac{1}{2} \int_0^a \left[t_1^w (w_0|_{y=0})^2 + t_3^w (w_0|_{y=b})^2 + t_1^v (v_0|_{y=0})^2 \right. \\ \left. + t_3^v (v_0|_{y=b})^2 + r_1 (\phi_y|_{y=0})^2 + r_3 (\phi_y|_{y=b})^2 \right] dx \\ + \frac{1}{2} \int_0^b \left[t_2^w (w_0|_{x=a})^2 + t_4^w (w_0|_{x=0})^2 + t_2^v (v_0|_{x=a})^2 \right. \\ \left. + t_4^v (v_0|_{x=0})^2 + r_2 (\phi_x|_{x=a})^2 + r_4 (\phi_x|_{x=0})^2 \right] dy, \end{aligned} \quad (11)$$

where t_i^* ($i = 1, \dots, 4$ and $\bullet = u, v, w$) are the elastic translational coefficients and r_i ($i = 1, \dots, 4$) are the elastic rotational coefficients.

The kinetic energy is expressed as

$$T = \frac{1}{2} \iint_R \left[I_0 (\dot{u}_0^2 + \dot{v}_0^2 + \dot{w}_0^2) + 2I_1 (\dot{u}_0 \phi_x + \dot{v}_0 \phi_y) + I_2 (\dot{\phi}_x^2 + \dot{\phi}_y^2) \right] dx dy, \quad (12)$$

being I_i ($i = 0, 1, 2$) the mass inertias of the plate defined as [35]

$$I_i = \int_{-h/2}^{h/2} \rho^{(k)} z^i dz, \quad (i = 0, 1, 2), \quad (13)$$

where $\rho^{(k)}$ is the material density of the k -th layer.

3. Application of the Ritz Method for the Free Vibration Analysis

The Ritz method is applied to determine analytical approximate solutions for dynamical behavior of arbitrarily laminated plates resting on elastic supports. During free vibration, the displacements components are assumed split in

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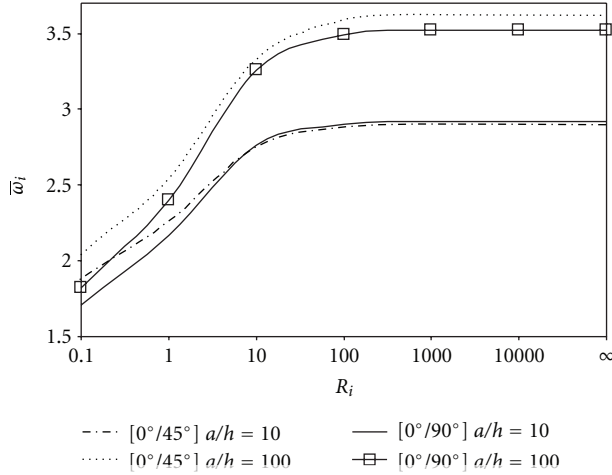


FIGURE 2: Variation of the fundamental frequency coefficient $\bar{\omega}$ with the rotational restraint parameter R_i , $T_i^w = T_i^u = T_i^v = \infty$ ($i = 1, \dots, 4$) for square $[0^\circ/45^\circ]$ and $[0^\circ/90^\circ]$ carbon-epoxy (Table 1), with $k_f = 0.6$.

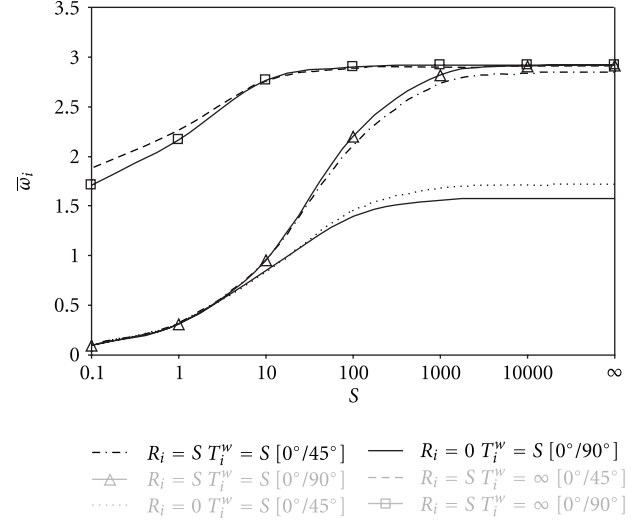


FIGURE 4: Variation of the fundamental frequency coefficient $\bar{\omega}$ with the translational and the rotational restraint parameters $T_i^w = R_i$, $T_i^u = T_i^v = 0$ ($i = 1, \dots, 4$) for square $[0^\circ/45^\circ]$ and $[0^\circ/90^\circ]$ carbon-epoxy (Table 1), with $k_f = 0.6$ and $a/h = 10$.

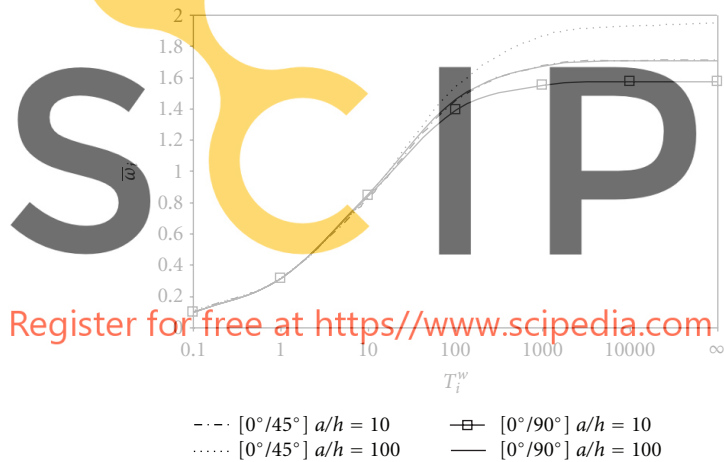


FIGURE 3: Variation of the fundamental frequency coefficient $\bar{\omega}$ with the translational restraint parameter T_i^w , $T_i^u = T_i^v = R_i = 0$ ($i = 1, \dots, 4$) for square $[0^\circ/45^\circ]$ and $[0^\circ/90^\circ]$ carbon-epoxy (Table 1), with $k_f = 0.6$.

the spatial and temporal parts, being the last one periodic in time; that is,

$$\begin{aligned} u_0(x, y, t) &= U(x, y) \sin \omega t, \\ v_0(x, y, t) &= V(x, y) \sin \omega t, \\ w_0(x, y, t) &= W(x, y) \sin \omega t, \\ \phi_x(x, y, t) &= \Phi_x(x, y) \sin \omega t, \\ \phi_y(x, y, t) &= \Phi_y(x, y) \sin \omega t, \end{aligned} \quad (14)$$

where ω is the natural frequency in radian. Putting these displacements into the energy functional components ((10) to (12)) the maximum values of the kinetic

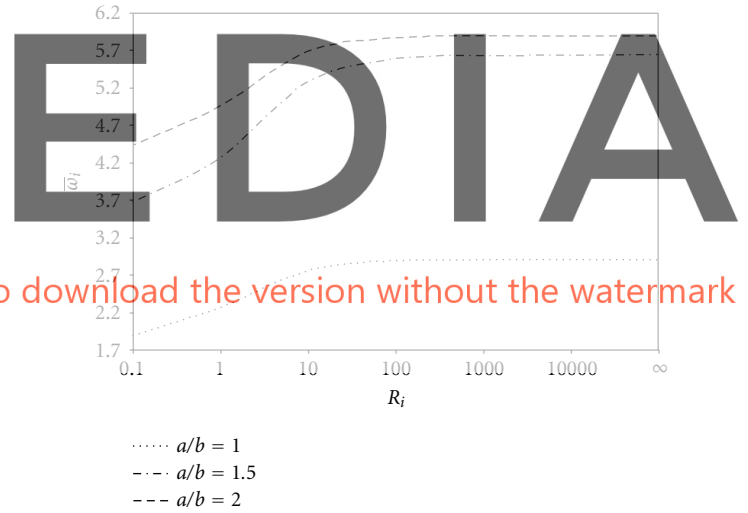


FIGURE 5: Variation of the fundamental frequency coefficient $\bar{\omega}$ with the rotational restraint parameter R_i , $T_i^w = T_i^u = T_i^v = \infty$ ($i = 1, \dots, 4$) for different aspect ratios $[0^\circ/45^\circ]$ carbon-epoxy (Table 1), with $k_f = 0.6$.

energy (T_{\max}) and the strain energies ($U_{p,\max}$, $U_{t,\max}$) are derived. Then, the energy functional for free vibration of the laminated plate is given by

$$\Pi = U_{p,\max} + U_{t,\max} - T_{\max}, \quad (15)$$

which is to be minimized according to the Ritz principle.

3.1. Boundary Conditions and Approximating Functions. There are some options when choosing the unknown functions of displacement components to apply the Ritz method. Particularly, the use of orthogonal polynomials as coordinate

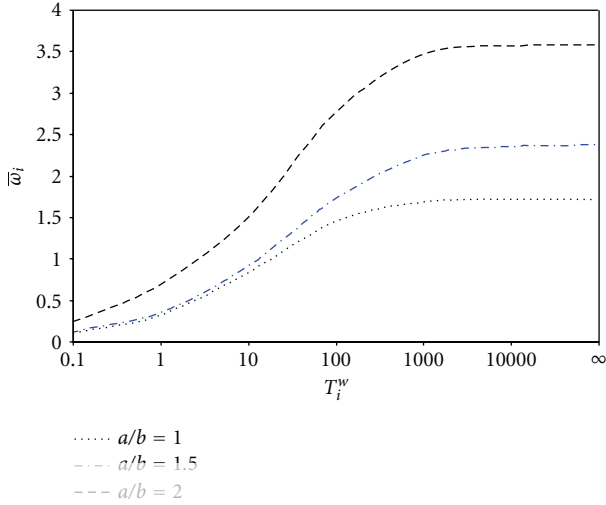


FIGURE 6: Variation of the fundamental frequency coefficient $\bar{\omega}$ with the translational restraint parameter T_i^w , $T_i^u = T_i^v = R_i = 0$ ($i = 1, \dots, 4$) for different aspect ratios $[0^\circ/45^\circ]$ carbon-epoxy (Table 1), with $k_f = 0.6$.

functions has important advantages related to numerical stability and fast convergence as has been demonstrated in previous works [23, 37, 38], even for plates with complicated boundary conditions and high degree of anisotropy. For these reasons, in this work, the displacement components are expressed by sets of beam characteristic orthogonal polynomials $\{p_i^{(\bullet)}(x)\}$, $\{q_j^{(\bullet)}(y)\}$, $(\bullet) = u, v, w, \phi_x, \phi_y$, resulting in

$$U(x, y) \approx U_{MN}(x, y) = \sum_{i=1}^M \sum_{j=1}^N c_{ij}^{(u)} p_i^{(u)}(x) q_j^{(u)}(y),$$

$$V(x, y) \approx V_{MN}(x, y) = \sum_{i=1}^M \sum_{j=1}^N c_{ij}^{(v)} p_i^{(v)}(x) q_j^{(v)}(y),$$

$$W(x, y) \approx W_{MN}(x, y) = \sum_{i=1}^M \sum_{j=1}^N c_{ij}^{(w)} p_i^{(w)}(x) q_j^{(w)}(y),$$

$$\Phi_x \approx \Phi_{xMN}(x, y) = \sum_{i=1}^N \sum_{j=1}^M c_{ij}^{(\phi_x)} p_i^{(\phi_x)}(x) q_j^{(\phi_x)}(y),$$

$$\Phi_y \approx \Phi_{yMN}(x, y) = \sum_{i=1}^N \sum_{j=1}^M c_{ij}^{(\phi_y)} p_i^{(\phi_y)}(x) q_j^{(\phi_y)}(y),$$

(16)

where $c_{ij}^{(u)}, c_{ij}^{(v)}, c_{ij}^{(w)}, c_{ij}^{(\phi_x)}, c_{ij}^{(\phi_y)}$ are the unknown coefficients, and M, N are the numbers of polynomials in each coordinate.

The procedure for the construction of the orthogonal polynomials has been developed by Bhat [39]. The first members of the sets, $p_1^{(\bullet)}(x)$ and $q_1^{(\bullet)}(y)$ ($\bullet = u, v, w, \phi_x, \phi_y$) are obtained as the simplest polynomials that satisfy all

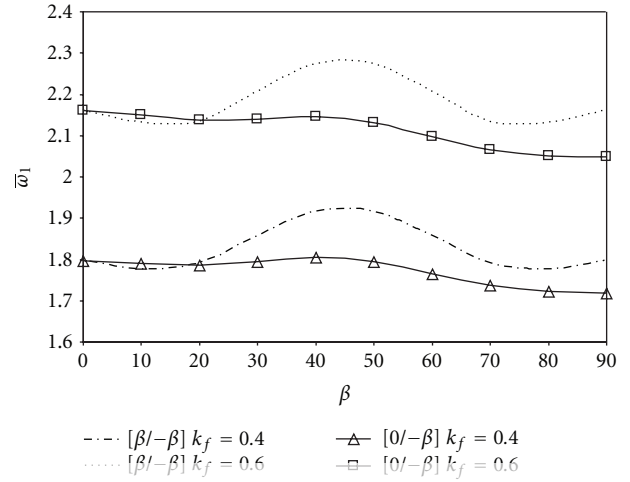


FIGURE 7: Effect of the fiber orientation on the first vibration frequency coefficient $\bar{\omega}_1$, for two different fiber volume fraction k_f with $C_1 C_1 C_1 C_1$ boundary condition and $a/h = 10$.

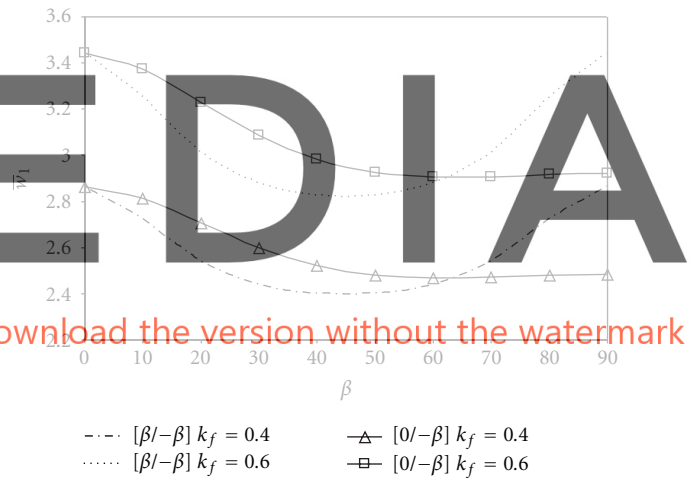


FIGURE 8: Effect of the fiber orientation on the first vibration frequency coefficient $\bar{\omega}_1$, for two different fiber volume fraction k_f with $S_1 S_1 S_1 S_1$ boundary condition and $a/h = 10$.

the geometrical boundary conditions of the plate in their respective x and y directions. The higher members of each set are constructed by employing the Gram-Schmidt orthogonalization procedure. The coefficients of the polynomials are chosen in such a way as to make the polynomials orthonormal. However, the functions $p_k^{(\bullet)}(x)$ and $q_k^{(\bullet)}(y)$ for $(\bullet) = \phi_x, \phi_y$ are obtained from relative rotation conditions starting from polynomials of an order lower than the chosen for the transversal displacements and then applying the sequence of Gram-Schmidt orthogonalization procedure. This particular choice is made to avoid the overestimation of the rate of elastic energy due to the shear respect to the rate due to the bending. This concept has been applied by Auciello and Ercolano [40], to Timoshenko beams, to avoid

TABLE 2: Notations for various combinations of boundary conditions, in which n and s indicate the directions normal and tangential to the respective plate edges.

Transverse constraints	In-plane constraints			
	$u_n = 0, u_s = 0$	$N_n = 0, u_s = 0$	$u_n = 0, N_{ns} = 0$	$N_n = 0, N_{ns} = 0$
Clamped: $w = 0; \phi_n = 0$	C_1	C_2	C_3	C_4
Simply supported: $w = 0; M_n = 0; \phi_s = 0$	S_1	S_2	S_3	S_4
Free: $M_n = 0; M_{ns} = 0; Q_n = 0$	F_1	F_2	F_3	F_4

TABLE 3: Convergence study of frequencies $\omega_i^* = \omega_i a^2 \sqrt{\rho/(E_2 h^2)}$ for a two-layered $[0^\circ/45^\circ]$ square plate. $E_1/E_2 = 25$, $G_{12} = G_{13} = 0.5E_2$, $G_{23} = 0.2E_2$, $\nu_{12} = 0.25$.

a/h	M, N ($M = N$)	Mode sequence number					
		1	2	3	4	5	6
10	4	15.487	23.582	30.182	35.243	42.217	49.098
	5	15.480	23.401	30.005	33.514	38.099	44.303
	6	15.478	23.359	29.960	33.217	37.825	43.331
	7	15.478	23.356	29.957	33.112	37.691	42.997
	8	15.478	23.356	29.956	33.104	37.679	42.901
	9	15.478	23.356	29.956	33.103	37.676	42.889
	10	15.478	23.356	29.956	33.103	37.675	42.887
	Shi et al. [5]	15.504	23.399	29.991	33.170	37.740	42.973
	4	19.248	30.947	42.338	50.788	71.618	81.985
	5	19.227	30.415	41.788	46.288	54.225	64.750
20	6	19.221	30.279	41.586	45.434	53.531	62.080
	7	19.219	30.271	41.572	45.047	53.090	61.032
	8	19.219	30.268	41.569	45.016	53.047	60.655
	9	19.218	30.267	41.569	45.008	53.032	60.600
	10	19.218	30.267	41.568	45.007	53.030	60.587
	Shi et al. [5]	19.350	30.490	41.769	45.400	53.385	61.035
	4	21.348	36.366	52.130	65.773	298.228	304.052
	5	21.314	35.002	50.893	56.783	68.251	86.403
	6	21.291	34.676	50.155	54.927	66.919	79.733
	7	21.289	34.660	50.124	53.854	65.602	76.972
100	8	21.288	34.655	50.107	53.792	65.504	75.800
	9	21.288	34.654	50.106	53.757	65.449	75.631
	10	21.288	34.654	50.106	53.754	65.444	75.553
	Shi et al. [5]	21.802	35.692	51.304	55.298	67.257	77.843

TABLE 4: Comparison of fundamental frequency coefficient $\omega_i^* = \omega_i a^2 \sqrt{\rho/(E_2 h^2)}$ for a four layered $[45^\circ/-45^\circ/45^\circ/-45^\circ]$ plate with different aspect ratios a/b . $E_1/E_2 = 40$, $G_{12} = 0.6E_2$, $G_{13} = G_{23} = 0.5E_2$, $\nu_{12} = 0.25$.

a/h		a/b						
		0.2	0.6	0.8	1	1.2	1.6	2
10	Present	9.013	13.02	15.74	18.62	21.59	27.66	34.57
	Alibeigloo et al. [31]	8.559	12.565	15.187	17.983	20.895	27.031	33.634
	Redy [32]	8.724	12.965	15.712	18.609	21.567	27.736	34.247
30	Present	9.965	15.409	19.293	23.638	28.377	39.062	51.480
	Alibeigloo et al. [31]	9.420	14.790	18.487	22.637	27.200	37.534	49.499
	Redy [32]	9.667	15.385	19.304	23.676	28.381	38.940	51.132
50	Present	10.056	15.66	19.70	24.25	29.25	40.70	54.25
	Alibeigloo et al. [31]	9.5016	15.0261	18.8586	23.195	28.003	39.05	52.686
	Redy [32]	9.816	15.689	19.759	24.343	29.321	40.653	53.989

TABLE 5: (a) Frequency parameters $\bar{\omega}_i$ for $[0^\circ/45^\circ]$ and $[0^\circ/90^\circ]$ carbon-epoxy AS4-3501-6 (Table 1), with different translational restraint parameter T_i^w , $T_i^u = T_i^v = R_i = 0$ ($i = 1, \dots, 4$), and $a/h = 10$. (b) Frequency parameters $\bar{\omega}_i$ for $[0^\circ/45^\circ]$ and $[0^\circ/90^\circ]$ carbon-epoxy AS4-3501-6 (Table 1), with different translational restraint parameter T_i^w , $T_i^u = T_i^v = R_i = 0$ ($i = 1, \dots, 4$), and $a/h = 100$.

(a)								
k_f	Mode	Translational restraint parameter T_i^w						
		0.1	1	10	100	1000	10000	1.00E + 10
$a/h = 10$								
$[0^\circ/45^\circ]$								
0.2	1	0.060	0.187	0.520	0.969	1.161	1.191	1.195
	2	0.085	0.266	0.803	1.827	2.380	2.470	2.481
	3	0.085	0.267	0.822	2.079	2.930	3.063	3.078
	4	0.754	0.810	1.224	2.609	3.776	4.004	4.032
0.4	1	0.083	0.256	0.689	1.219	1.419	1.448	1.452
	2	0.117	0.367	1.083	2.284	2.829	2.912	2.922
	3	0.117	0.368	1.125	2.723	3.638	3.767	3.782
	4	0.890	0.978	1.590	3.325	4.530	4.735	4.759
0.6	1	0.101	0.310	0.824	1.443	1.671	1.705	1.709
	2	0.142	0.445	1.303	2.685	3.290	3.382	3.393
	3	0.142	0.447	1.364	3.274	4.342	4.492	4.509
	4	1.040	1.151	1.903	3.936	5.292	5.517	5.543
$[0^\circ/90^\circ]$								
0.2	1	0.060	0.188	0.528	0.942	1.084	1.104	1.106
	2	0.085	0.267	0.814	1.970	2.657	2.756	2.768
	3	0.085	0.267	0.814	1.970	2.657	2.756	2.768
	4	0.628	0.697	1.164	2.642	3.708	3.888	3.909
0.4	1	0.083	0.258	0.705	1.181	1.321	1.340	1.342
	2	0.117	0.368	1.110	2.546	3.251	3.344	3.355
	3	0.117	0.368	1.110	2.546	3.251	3.344	3.355
	4	0.750	0.858	1.540	3.424	4.519	4.675	4.675
0.6	1	0.101	0.313	0.847	1.395	1.553	1.574	1.577
	2	0.142	0.446	1.343	3.035	3.829	3.932	3.944
	3	0.142	0.446	1.343	3.035	3.829	3.932	3.944
	4	0.910	1.040	1.864	4.089	5.329	5.514	5.536

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(b)								
k_f	Mode	Translational restraint parameter T_i^w						
		0.1	1	10	100	1000	10000	1.00E + 10
$a/h = 100$								
$[0^\circ/45^\circ]$								
0.2	1	0.060	0.187	0.525	1.014	1.276	1.329	1.340
	2	0.085	0.268	0.813	1.928	2.708	2.881	2.908
	3	0.085	0.269	0.832	2.214	3.489	3.771	3.815
	4	0.804	0.858	1.266	2.774	4.519	5.027	5.098
0.4	1	0.083	0.256	0.697	1.292	1.577	1.633	1.646
	2	0.117	0.369	1.099	2.445	3.269	3.440	3.468
	3	0.117	0.370	1.142	2.952	4.444	4.746	4.794
	4	0.947	1.032	1.642	3.588	5.531	6.011	6.073
0.6	1	0.101	0.310	0.835	1.531	1.859	1.925	1.940
	2	0.142	0.447	1.324	2.880	3.804	3.995	4.028
	3	0.143	0.450	1.385	3.555	5.304	5.654	5.711
	4	1.104	1.210	1.962	4.255	6.457	6.980	7.046

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(b) Continued.

k_f	Mode	Translational restraint parameter T_i^w						
		0.1	1	10	100	1000	10000	1.00E + 10
	[0°/90°]							
0.2	1	0.060	0.188	0.533	0.981	1.161	1.190	1.194
	2	0.085	0.268	0.823	2.086	3.043	3.212	3.233
	3	0.085	0.268	0.823	2.086	3.043	3.212	3.233
	4	0.666	0.732	1.197	2.805	4.365	4.732	4.782
0.4	1	0.083	0.258	0.714	1.239	1.422	1.449	1.453
	2	0.117	0.370	1.126	2.738	3.783	3.948	3.969
	3	0.117	0.370	1.126	2.738	3.783	3.948	3.969
	4	0.797	0.901	1.583	3.699	5.418	5.774	5.821
0.6	1	0.101	0.313	0.857	1.464	1.674	1.706	1.710
	2	0.143	0.449	1.363	3.271	4.453	4.638	4.661
	3	0.143	0.449	1.363	3.271	4.453	4.638	4.661
	4	0.967	1.093	1.917	4.427	6.392	6.797	6.851

the shear locking effect and is extended here for laminated plates.

The classical boundary conditions considered in this study are depicted in Table 2. By keeping in mind that in the Ritz method only the geometric boundary conditions need to be satisfied, it is possible to work with any sets of required edge boundary condition and also is very simple the consideration of elastically restrained edges where there are not essential boundary conditions to satisfy.

Upon inserting the displacement forms (16) into the energy functional of the system (15), the minimization with respect to the coefficients of the displacement functions is given by

$$\begin{aligned} \frac{\partial \Pi}{\partial c_{ij}^{(u)}} = 0, \quad \frac{\partial \Pi}{\partial c_{ij}^{(v)}} = 0, \quad \frac{\partial \Pi}{\partial c_{ij}^{(w)}} = 0, \\ \frac{\partial \Pi}{\partial c_{ij}^{(\phi_x)}} = 0, \quad \frac{\partial \Pi}{\partial c_{ij}^{(\phi_y)}} = 0. \end{aligned} \quad (17)$$

From (17) a set of algebraic simultaneous equations is obtained. The number of these equations becomes $5 \times M \times N$. The algebraic equations obtained are given as follows, in the form of the generalized eigenvalue problem:

$$(\mathbf{K} - \omega^2 \mathbf{M})\{\mathbf{C}\} = \{\mathbf{0}\}, \quad (18)$$

where \mathbf{K} and \mathbf{M} are stiffness and inertia matrices, respectively (their expressions are given in the Appendix, $\{\mathbf{C}\}$ contains the unknown coefficients of (16).

For a nontrivial solution, the eigenvalues which make the determinant equal to zero, correspond to the free vibration frequencies.

4. Verification of the Formulation and Numerical Applications

4.1. General Description. The variational algorithm developed in this paper was programmed in Fortran language and

used for the free vibration analysis of generally laminated thin and moderately thick laminated plates having different geometric parameters, stacking sequences, material properties, fiber volume fractions, and boundary conditions. The examples considered in this study are confined to laminates with layers of equal thickness, even though the procedure was formulated for plies with arbitrary thickness. In all cases the shear correction factor was taken a 5/6.

Let us introduce the terminology to be used throughout the remainder of the paper for describing the boundary conditions of the considered plates. The designation $C_i S_i F_i S_i$, for example, identifies a plate with edges (1) clamped, (2) simply supported, (3) free, and (4) simply supported (see Figure 1) for the cases $i = 1, 2, 3, 4$ and $v = u, v, w$ in plane constraints according to Table 2. When the edges are elastically restrained against rotation or translation, the following nondimensional restraint parameters are used

$$T_i^\bullet = \frac{a^3 t_i^\bullet}{D_0}, \quad (i = 1, \dots, 4 \text{ and } \bullet = u, v, w), \quad (19)$$

$$R_i = \frac{r_i a}{D_0}, \quad (i = 1, \dots, 4),$$

where $D_0 = E_1 h^3 / 12(1 - \nu_{12} \nu_{21})$.

The main purposes of the numerical applications presented in this section are twofold. One is to demonstrate the accuracy, the flexibility, and the efficiency of the proposed method and the other is to produce some results which may be regarded as benchmark solutions for other academic research workers and design engineers.

4.2. Validation and Convergence Studies. The accuracy and reliability of the results obtained with the present approach are next demonstrated by comparing them with some selected values published by Shi et al. [5] for moderately thick ($a/h = 10, 20$) and thin ($a/h = 100$) arbitrarily clamped laminated plates. The comparison presented in Table 3 authenticates the validity of the present method for arbitrarily laminated plates. Very close agreement for the first

TABLE 6: (a) Frequency parameters $\bar{\omega}_i$ for $[0^\circ/45^\circ]$ and $[0^\circ/90^\circ]$ carbon-epoxy AS4-3501-6 (Table 1), with different rotational restraint parameter R_i , $T_i^w = T_i^u = T_i^v = \infty$ ($i = 1, \dots, 4$), and $a/h = 10$. (b) Frequency parameters $\bar{\omega}_i$ for $[0^\circ/45^\circ]$ and $[0^\circ/90^\circ]$ carbon-epoxy AS4-3501-6 (Table 1), with different rotational restraint parameter R_i , $T_i^w = T_i^u = T_i^v = \infty$ ($i = 1, \dots, 4$), and $a/h = 100$.

(a)								
k_f	Mode	Rotational restraint parameter R_i						
		0.1	1	10	100	1000	10000	1.00E + 10
$a/h = 10$								
$[0^\circ/45^\circ]$								
0.2	1	1.461	1.623	1.943	2.056	2.071	2.072	2.072
	2	2.709	2.903	3.268	3.390	3.406	3.407	3.407
	3	3.350	3.497	3.861	4.010	4.030	4.032	4.032
	4	4.322	4.477	4.818	4.951	4.969	4.971	4.971
0.4	1	1.837	2.029	2.371	2.483	2.497	2.498	2.498
	2	3.249	3.493	3.875	3.988	4.002	4.003	4.003
	3	4.112	4.302	4.709	4.854	4.872	4.874	4.874
	4	5.129	5.333	5.700	5.823	5.838	5.840	5.840
0.6	1	2.182	2.408	2.803	2.931	2.947	2.949	2.949
	2	3.799	4.090	4.527	4.654	4.669	4.671	4.671
	3	4.884	5.119	5.611	5.783	5.804	5.806	5.807
	4	5.987	6.239	6.672	6.812	6.830	6.832	6.832
$[0^\circ/90^\circ]$								
0.2	1	1.386	1.562	1.916	2.034	2.048	2.050	2.050
	2	2.901	3.110	3.561	3.719	3.738	3.740	3.741
	3	2.901	3.110	3.561	3.719	3.738	3.740	3.741
	4	4.052	4.287	4.764	4.970	4.994	4.996	4.996
0.4	1	1.755	1.969	2.352	2.468	2.482	2.483	2.483
	2	3.532	3.814	4.321	4.473	4.491	4.493	4.493
	3	3.532	3.814	4.321	4.473	4.491	4.493	4.493
	4	4.932	5.218	5.745	5.949	5.971	5.973	5.973
0.6	1	2.090	2.340	2.776	2.905	2.920	2.922	2.922
	2	4.167	4.511	5.102	5.272	5.292	5.294	5.295
	3	4.167	4.511	5.102	5.272	5.292	5.294	5.295
	4	5.833	6.179	6.790	7.021	7.045	7.047	7.048

(b)								
k_f	Mode	Rotational restraint parameter R_i						
		0.1	1	10	100	1000	10000	1.00E + 10
$a/h = 100$								
$[0^\circ/45^\circ]$								
0.2	1	1.598	1.814	2.318	2.534	2.564	2.567	2.567
	2	3.108	3.410	4.115	4.415	4.457	4.461	4.462
	3	4.161	4.421	5.275	5.759	5.831	5.839	5.840
	4	5.366	5.689	6.611	7.100	7.173	7.181	7.181
0.4	1	2.044	2.316	2.901	3.135	3.166	3.169	3.170
	2	3.783	4.185	4.997	5.311	5.353	5.358	5.358
	3	5.265	5.627	6.699	7.240	7.317	7.325	7.326
	4	6.450	6.911	8.018	8.523	8.594	8.601	8.602
0.6	1	2.428	2.748	3.423	3.689	3.725	3.729	3.729
	2	4.418	4.896	5.821	6.171	6.217	6.222	6.223
	3	6.250	6.692	7.967	8.593	8.682	8.691	8.692
	4	7.498	8.058	9.337	9.897	9.974	9.983	9.983

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(b) Continued.

k_f	Mode	Rotational restraint parameter R_i						
		0.1	1	10	100	1000	10000	1.00E + 10
	[0°/90°]							
0.2	1	1.493	1.719	2.223	2.413	2.437	2.440	2.440
	2	3.396	3.720	4.583	4.960	5.010	5.016	5.016
	3	3.396	3.720	4.583	4.960	5.010	5.016	5.016
	4	5.036	5.390	6.396	6.966	7.039	7.047	7.048
0.4	1	1.917	2.203	2.780	2.976	3.001	3.003	3.003
	2	4.202	4.665	5.725	6.122	6.172	6.178	6.178
	3	4.202	4.665	5.725	6.122	6.172	6.178	6.178
	4	6.173	6.688	7.937	8.560	8.634	8.641	8.642
0.6	1	2.286	2.621	3.277	3.494	3.521	3.523	3.524
	2	4.952	5.515	6.745	7.185	7.241	7.247	7.247
	3	4.952	5.515	6.745	7.185	7.241	7.247	7.247
	4	7.297	7.918	9.364	10.060	10.141	10.149	10.150

sixth nondimensional frequencies $\omega_i^* = \omega_i a^2 \sqrt{\rho/(E_2 h^2)}$ is obtained for all cases and display monotonic convergence tendency to constant values. For thick plates, as shown in Table 3, as number of N and M is increased from 7 to 10, the frequency parameter decreases merely 0.002% for the first mode and 0.26% for the sixth. For thin plates the relative decreases of the frequency parameters are 0.004% for the first mode and 1.88% for the sixth as the numbers of polynomials M, N are increased from 7 to 10, exhibiting slower convergence rate than that of moderately thick plates. Consequently the number of beam characteristic polynomials used in the following computations for thin and thick plates is chosen as

The validation of the proposed methodology for different aspect ratios (a/b) is presented in Table 4, showing a good agreement with Alibeigloo et al. [31] and Reddy [32].

4.3. Numerical Results and Discussion. Several examples including new results for arbitrarily laminated plates with elastically restrained edges are presented in this section. The elastic properties of the composite materials used here are those shown in Table 1. The influence of different values of fiber volume ratios (k_f) is analyzed in several figures and tables.

Values of the first four frequency parameters $\bar{\omega}_i = \omega_i(a^2/h)\sqrt{\rho/E_{f1}}$ for square thick ($a/h = 10$) and thin ($a/h = 100$) unsymmetric laminated plates are shown for increasing values of the translational restraint parameter T_i^w , in Tables 5(a) and 5(b). Moreover, the influence of rotational restraint parameter R_i in the free vibration frequency coefficients is shown in Tables 6(a) and 6(b).

In Figures 2–4 the fundamental frequency coefficients $\bar{\omega}$ corresponding to two laminated square plates are plotted against the restraint parameters R_i and T_i^w . Figure 2 shows the variation of $\bar{\omega}$ for various values of the rotational restraint R_i , while Figure 3 shows the variation of $\bar{\omega}$ for various values of the translational restraint T_i^w . A major increase of frequency occurs when the elastic restraint values are in

the interval 0.1–50. Figure 4 shows the variation of $\bar{\omega}$ for various values of the rotational and translational restraint parameters: (a) $R_i = 0, T_i^w = S$; (b) $R_i = S, T_i^w = \infty$, and (c) $R_i = T_i^w = S$. The obtained curves illustrate the restraint parameters intervals for which the frequency coefficient $\bar{\omega}$ is sensitive to R_i and T_i^w .

To assess the influence of the aspect ratio a/b in the laminated plate response, values of the first four frequency parameters $\bar{\omega}_i = \omega_i(a^2/h)\sqrt{\rho/E_{f1}}$ for rectangular thick ($a/h = 10$) unsymmetric laminated plates are shown, for increasing values of the translational restraint parameter T_i^w (Table 7(a)) and the rotational restraint parameter R_i (Table 7(b)) considering $a/b = 1.5$ and $a/b = 2$.

Figure 5 shows the variation of $\bar{\omega}$ for various values of the rotational restraint R_i , while Figure 6 shows the variation of $\bar{\omega}$ for various values of the translational restraint T_i^w for rectangular laminated plates.

To evaluate the effect of different fiber orientation angles (β) and fiber volume fraction on the dynamic properties of the laminates, the variation of the first free vibration coefficient $\bar{\omega}_1$ is plotted in Figures 7 and 8, considering two lamination stacking sequences, $[\beta/-\beta]$ and $[0/\beta]$. Two boundary conditions have been included, $C_1C_1C_1C_1$ in Figure 7 and $S_1S_1S_1S_1$ in Figure 6. It is observed that the $[\beta/-\beta]$ laminate is more sensitive to the fiber orientation angle than $[0/\beta]$ lamination scheme. The adimensional frequency parameter is noticeable higher as the fiber volume fraction k_f increases and as the boundary conditions become clamped.

Finally, the first four free vibration coefficients are presented in Table 8 to illustrate the influence of various fiber volume fractions and boundary conditions on the dynamical behavior of an unsymmetric $[0^\circ/45^\circ]$ laminated plate.

5. Concluding Remarks

A Ritz approach for free vibration analysis of general laminated plates with edges elastically restrained against translation and rotation is presented in this work. The study

TABLE 7: (a) Frequency parameters $\bar{\omega}_i$ for $[0^\circ/45^\circ]$ carbon-epoxy AS4-3501-6 (Table 1), with different translational restraint parameter T_i^w , $T_i^u = T_i^v = R_i = 0$ ($i = 1, \dots, 4$), and $a/h = 10$. (b) Frequency parameters $\bar{\omega}_i$ for $[0^\circ/45^\circ]$ carbon-epoxy AS4-3501-6 (Table 1), with different rotational restraint parameter R_i , $T_i^u = T_i^v = T_i^w = \infty$ ($i = 1, \dots, 4$), and $a/h = 10$.

(a)								
k_f	Mode	Translational restraint parameter T_i^w						
		0.1	1	10	100	1000	10000	1.00E + 10
$a/b = 2$								
0.2	1	0.158	0.464	1.043	2.045	2.778	2.903	2.917
	2	0.184	0.574	1.625	3.592	4.520	4.704	4.726
	3	0.255	0.793	2.167	3.948	6.915	7.139	7.149
	4	1.652	1.823	2.838	5.127	7.177	7.419	7.449
0.4	1	0.199	0.578	1.268	2.392	3.046	3.144	3.156
	2	0.233	0.723	1.999	4.175	5.024	5.169	5.186
	3	0.322	0.999	2.649	4.774	7.759	8.125	8.148
	4	1.832	2.071	3.374	6.021	7.973	8.173	8.196
0.6	1	0.235	0.681	1.487	2.757	3.455	3.557	3.569
	2	0.275	0.853	2.347	4.837	5.763	5.915	5.933
	3	0.380	1.179	3.115	5.589	8.864	9.309	9.342
	4	2.104	2.394	3.945	6.992	9.186	9.408	9.434
$a/b = 1.5$								
0.2	1	0.111	0.341	0.904	1.724	2.239	2.345	2.364
	2	0.141	0.443	1.335	3.326	4.739	5.023	5.067
	3	0.171	0.539	1.627	3.705	5.946	6.580	6.673
	4	1.423	1.542	2.285	4.768	7.832	8.845	8.980
0.4	1	0.140	0.429	1.108	2.012	2.501	2.598	2.617
	2	0.178	0.559	1.664	3.964	5.396	5.649	5.686
	3	0.216	0.681	2.037	4.480	6.688	7.229	7.313
	4	1.587	1.731	2.729	5.680	8.857	9.749	9.869
0.6	1	0.165	0.506	1.296	2.316	2.847	2.954	2.976
	2	0.210	0.660	1.957	4.587	6.194	6.469	6.509
	3	0.256	0.804	2.400	5.243	7.625	8.198	8.292
	4	1.815	1.989	3.182	6.582	10.085	11.034	11.163
(b)								
k_f	Mode	Rotational restraint parameter $R_i^{\phi_x, \phi_y}$						
		0.1	1	10	100	1000	10000	1.00E + 10
$a/b = 2$								
0.2	1	3.444	3.858	4.588	4.806	4.833	4.835	4.836
	2	5.467	5.742	6.278	6.450	6.472	6.474	6.474
	3	8.161	8.349	8.750	8.890	8.908	8.909	8.910
	4	8.357	8.741	9.485	9.722	9.751	9.754	9.754
0.4	1	3.854	4.314	4.989	5.183	5.183	5.185	5.186
	2	6.061	6.362	6.855	7.009	7.009	7.011	7.011
	3	8.971	9.187	9.552	9.678	9.678	9.680	9.680
	4	8.987	9.437	10.142	10.37	10.347	10.349	10.349
0.6	1	4.421	4.946	5.682	5.866	5.887	5.889	5.889
	2	6.961	7.309	7.858	8.006	8.024	8.026	8.026
	3	10.160	10.584	10.999	11.124	11.139	11.140	11.141
	4	10.352	10.720	11.512	11.709	11.732	11.734	11.735

(b) Continued.

k_f	Mode	Rotational restraint parameter $R_i^{\phi_x, \phi_y}$						
		0.1	1	10	100	1000	10000	1.00E + 10
$a/b = 1.5$								
0.2	1	2.764	3.203	4.114	4.438	4.479	4.483	4.484
	2	5.686	6.122	7.270	7.771	7.839	7.846	7.847
	3	7.047	7.669	9.272	9.946	10.035	10.045	10.046
	4	9.588	10.107	11.673	12.471	12.586	12.598	12.599
0.4	1	3.188	3.703	4.631	4.925	4.961	4.965	4.966
	2	6.470	7.016	8.260	8.739	8.801	8.807	8.808
	3	7.847	8.632	10.324	10.927	11.003	11.011	11.012
	4	10.679	11.329	13.007	13.742	13.843	13.853	13.854
0.6	1	3.663	4.252	5.272	5.585	5.624	5.628	5.628
	2	7.394	8.040	9.448	9.973	10.040	10.047	10.048
	3	8.920	9.842	11.721	12.360	12.440	12.448	12.449
	4	12.113	12.873	14.748	15.537	15.643	15.654	15.655

TABLE 8: Frequency parameters $\bar{\omega}_i$ for $[0^\circ/45^\circ]$ carbon-epoxy AS4-3501-6 (Table 1), with different fiber volume fraction k_f and boundary conditions. $a/h = 10$.

Boundary conditions	k_f	Mode sequence number			
		1	2	3	4
$S_1 S_1 S_1 S_1$	0.1	1.198	2.379	0.193	2.872
	0.2	1.435	2.683	0.166	3.337
	0.3	1.628	2.951	0.154	3.723
	0.4	1.804	3.212	0.148	4.092
	0.5	1.973	3.475	0.145	4.463
	0.6	2.143	3.754	0.145	4.859
	0.7	2.319	4.054	0.146	5.290
	0.8	2.489	4.344	0.148	5.724
$C_1 C_1 C_1 C_1$	0.1	1.826	3.091	3.560	4.502
	0.2	2.073	3.407	4.032	4.961
	0.3	2.287	3.702	4.452	5.387
	0.4	2.498	4.003	4.874	5.824
	0.5	2.715	4.321	5.317	6.290
	0.6	2.949	4.671	5.807	6.809
	0.7	3.207	5.062	6.359	7.396
	0.8	3.466	5.449	6.934	7.982
$S_2 S_2 C_1 C_1$	0.1	1.446	2.825	3.037	3.975
	0.2	1.651	3.137	3.469	4.621
	0.3	1.830	3.417	3.847	5.045
	0.4	2.002	3.697	4.213	5.470
	0.5	2.173	3.987	4.587	5.912
	0.6	2.351	4.303	4.989	6.395
	0.7	2.541	4.651	5.430	6.933
	0.8	2.724	4.989	5.876	7.464

includes the effective elastic moduli of each lamina obtained using the Mori-Tanaka mean field theory, which allows taking into account the influence of the fiber volume ratios and the elastic properties of the components (fiber and matrix) into the vibration behavior. The formulation is based on

the first-order shear deformation theory, and the generalized displacements are approximate using sets of characteristic orthogonal polynomials generated by the Gram-Schmidt procedure. The consideration of all possible rotational and translational restraints allows generating any classical

boundary condition, only approaching the corresponding spring parameter to zero or infinity. The algorithm is computationally efficient, and the solutions are stables and convergent. Close agreement with existing results in the literature is shown and new results are presented in tables and figures which could be useful for design and optimization problems of general long fiber-reinforced laminated plates.

Appendix

The matrices K and M in (18) are given by

$$[\mathbf{K}] = \begin{bmatrix} [K_{ijkh}^{uu}] & [K_{ijkh}^{uv}] & [K_{ijkh}^{uw}] & [K_{ijkh}^{u\phi_x}] & [K_{ijkh}^{u\phi_y}] \\ & [K_{ijkh}^{vv}] & [K_{ijkh}^{vw}] & [K_{ijkh}^{v\phi_x}] & [K_{ijkh}^{v\phi_y}] \\ & & [K_{ijkh}^{ww}] & [K_{ijkh}^{w\phi_x}] & [K_{ijkh}^{w\phi_y}] \\ & & & [K_{ijkh}^{\phi_x\phi_x}] & [K_{ijkh}^{\phi_x\phi_y}] \\ \text{sym} & & & & [K_{ijkh}^{\phi_y\phi_y}] \end{bmatrix}, \quad (\text{A.1})$$

where

$$\begin{aligned} 3K_{ijkh}^{uu} &= A_{11} \iint_R p_i^{(u)} p_k^{(u)} q_j^{(u)} q_h^{(u)} dx dy \\ &+ A_{16} \iint_R (p_i^{(u)} p_k^{(u)} q_j^{(u)} q_h^{(u)} q_h^{(u)}) \\ &\quad + p_i^{(u)} p_k^{(u)} q_j^{(u)} q_h^{(u)}) dx dy \\ &+ A_{66} \iint_R p_i^{(u)} p_k^{(u)} q_j^{(u)} q_h^{(u)} dx dy \\ &+ t_2^u \int_0^b [p_i^{(u)} p_k^{(u)}]_{x=1} q_j^{(u)} q_h^{(u)} dy \\ &+ t_4^u \int_0^b [p_i^{(u)} p_k^{(u)}]_{x=0} q_j^{(u)} q_h^{(u)} dy, \\ K_{ijkh}^{uv} &= A_{12} \iint_R p_i^{(u)} p_k^{(v)} q_j^{(u)} q_h^{(v)} dx dy \\ &+ A_{16} \iint_R p_i^{(v)} p_k^{(u)} q_j^{(v)} q_h^{(u)} dx dy \\ &+ A_{26} \iint_R p_i^{(v)} p_k^{(u)} q_j^{(v)} q_h^{(u)} dx dy \\ &+ A_{66} \iint_R p_i^{(v)} p_k^{(u)} q_j^{(v)} q_h^{(u)} dx dy, \\ K_{ijkh}^{uw} &= 0, \quad K_{ijkh}^{vw} = 0, \end{aligned}$$

$$\begin{aligned} K_{ijkh}^{u\phi_x} &= B_{11} \iint_R p_i^{(u)} p_k^{(\phi_x)} q_j^{(u)} q_h^{(\phi_x)} dx dy \\ &+ B_{16} \iint_R p_i^{(u)} p_k^{(\phi_x)} q_j^{(u)} q_h^{(\phi_x)} dx dy \\ &+ B_{16} \iint_R p_i^{(u)} p_k^{(\phi_x)} q_j^{(u)} q_h^{(\phi_x)} dx dy \\ &+ B_{66} \iint_R p_i^{(u)} p_k^{(\phi_x)} q_j^{(u)} q_h^{(\phi_x)} dx dy, \\ K_{ijkh}^{u\phi_y} &= B_{12} \iint_R p_i^{(u)} p_k^{(\phi_y)} q_j^{(u)} q_h^{(\phi_y)} dx dy \\ &+ B_{16} \iint_R p_i^{(u)} p_k^{(\phi_y)} q_j^{(u)} q_h^{(\phi_y)} dx dy \\ &+ B_{26} \iint_R p_i^{(u)} p_k^{(\phi_y)} q_j^{(u)} q_h^{(\phi_y)} dx dy \\ &+ B_{66} \iint_R p_i^{(u)} p_k^{(\phi_y)} q_j^{(u)} q_h^{(\phi_y)} dx dy, \\ K_{ijkh}^{vv} &= A_{22} \iint_R p_i^{(v)} p_k^{(v)} q_j^{(v)} q_h^{(v)} dx dy \\ &+ A_{26} \iint_R (p_i^{(v)} p_k^{(v)} q_j^{(v)} q_h^{(v)} \\ &\quad + p_i^{(v)} p_k^{(v)} q_j^{(v)} q_h^{(v)}) dx dy \\ &+ A_{66} \iint_R p_i^{(v)} p_k^{(v)} q_j^{(v)} q_h^{(v)} dx dy \\ &+ t_1^v \int_0^a p_i^{(v)} p_k^{(v)} [q_j^{(v)} q_h^{(v)}]_{y=0} dx \\ &+ t_3^v \int_0^b p_i^{(v)} p_k^{(v)} [q_j^{(v)} q_h^{(v)}]_{y=1} dx, \\ K_{ijkh}^{v\phi_x} &= B_{12} \iint_R p_i^{(v)} p_k^{(\phi_x)} q_j^{(v)} q_h^{(\phi_x)} dx dy \\ &+ B_{16} \iint_R p_i^{(v)} p_k^{(\phi_x)} q_j^{(v)} q_h^{(\phi_x)} dx dy \\ &+ B_{26} \iint_R p_i^{(v)} p_k^{(\phi_x)} q_j^{(v)} q_h^{(\phi_x)} dx dy \\ &+ B_{66} \iint_R p_i^{(v)} p_k^{(\phi_x)} q_j^{(v)} q_h^{(\phi_x)} dx dy, \\ K_{ijkh}^{v\phi_y} &= B_{22} \iint_R p_i^{(v)} p_k^{(\phi_y)} q_j^{(v)} q_h^{(\phi_y)} dx dy \\ &+ B_{26} \iint_R p_i^{(v)} p_k^{(\phi_y)} q_j^{(v)} q_h^{(\phi_y)} dx dy \\ &+ B_{26} \iint_R p_i^{(v)} p_k^{(\phi_y)} q_j^{(v)} q_h^{(\phi_y)} dx dy \\ &+ B_{66} \iint_R p_i^{(v)} p_k^{(\phi_y)} q_j^{(v)} q_h^{(\phi_y)} dx dy, \end{aligned}$$

$$\begin{aligned}
K_{ijkh}^{ww} = & A_{44} \iint_R p_i^{(w)} p_k^{(w)} q_j^{(w)} q_h^{(w)} dx dy \\
& + A_{55} \iint_R p_i^{(w)} p_k^{(w)} q_j^{(w)} q_h^{(w)} dx dy \\
& + A_{45} \iint_R (p_i^{(w)} p_k^{(w)} q_j^{(w)} q_h^{(w)} \\
& \quad + p_i^{(w)} p_k^{(w)} q_j^{(w)} q_h^{(w)}) dx dy \\
& + t_1^w \int_0^a p_i^{(w)} p_k^{(w)} [q_j^{(w)} q_h^{(w)}]_{y=0} dx \\
& + t_2^w \int_0^b [p_i^{(w)} p_k^{(w)}]_{x=1} q_j^{(w)} q_h^{(w)} dy \\
& + t_3^w \int_0^a p_i^{(w)} p_k^{(w)} [q_j^{(w)} q_h^{(w)}]_{y=1} dx \\
& + t_4^w \int_0^b [p_i^{(w)} p_k^{(w)}]_{x=0} q_j^{(w)} q_h^{(w)} dy,
\end{aligned}$$

$$\begin{aligned}
K_{ijkh}^{w\phi_x} = & K \left(A_{45} \iint_R p_i^{(w)} p_k^{(\phi_x)} q_j^{(w)} q_h^{(\phi_x)} dx dy \right. \\
& \left. + A_{55} \iint_R p_i^{(w)} p_k^{(\phi_x)} q_j^{(w)} q_h^{(\phi_x)} dx dy \right),
\end{aligned}$$

$$\begin{aligned}
K_{ijkh}^{w\phi_y} = & K \left(A_{44} \iint_R p_i^{(w)} p_k^{(\phi_y)} q_j^{(w)} q_h^{(\phi_y)} dx dy \right. \\
& \left. + A_{45} \iint_R p_i^{(w)} p_k^{(\phi_y)} q_j^{(w)} q_h^{(\phi_y)} dx dy \right),
\end{aligned}$$

$$\begin{aligned}
K_{ijkh}^{\phi_x\phi_x} = & KA_{55} \iint_R p_i^{(\phi_x)} p_k^{(\phi_x)} q_j^{(\phi_x)} q_h^{(\phi_x)} dx dy \\
& + D_{11} \iint_R p_i^{(\phi_x)} p_k^{(\phi_x)} q_j^{(\phi_x)} q_h^{(\phi_x)} dx dy \\
& + D_{16} \iint_R (p_i^{(\phi_x)} p_k^{(\phi_x)} q_j^{(\phi_x)} q_h^{(\phi_x)} \\
& \quad + p_i^{(\phi_x)} p_k^{(\phi_x)} q_j^{(\phi_x)} q_h^{(\phi_x)}) dx dy \\
& + D_{66} \iint_R p_i^{(\phi_x)} p_k^{(\phi_x)} q_j^{(\phi_x)} q_h^{(\phi_x)} dx dy \\
& + r_2 \int_0^b [p_i^{(\phi_x)} p_k^{(\phi_x)}]_{x=a} q_j^{(\phi_x)} q_h^{(\phi_x)} dy \\
& + r_4 \int_0^b [p_i^{(\phi_x)} p_k^{(\phi_x)}]_{x=0} q_j^{(\phi_x)} q_h^{(\phi_x)} dy,
\end{aligned}$$

$$\begin{aligned}
K_{ijkh}^{\phi_x\phi_y} = & KA_{45} \iint_R p_i^{(\phi_x)} p_k^{(\phi_y)} q_j^{(\phi_x)} q_h^{(\phi_y)} dx dy \\
& + D_{12} \iint_R p_i^{(\phi_x)} p_k^{(\phi_y)} q_j^{(\phi_x)} q_h^{(\phi_y)} dx dy \\
& + D_{16} \iint_R p_i^{(\phi_x)} p_k^{(\phi_y)} q_j^{(\phi_x)} q_h^{(\phi_y)} dx dy \\
& + D_{26} \iint_R p_i^{(\phi_x)} p_k^{(\phi_y)} q_j^{(\phi_x)} q_h^{(\phi_y)} dx dy \\
& + D_{66} \iint_R p_i^{(\phi_x)} p_k^{(\phi_y)} q_j^{(\phi_x)} q_h^{(\phi_y)} dx dy,
\end{aligned}$$

$$\begin{aligned}
K_{ijkh}^{\phi_y\phi_y} = & KA_{44} \iint_R p_i^{(\phi_y)} p_k^{(\phi_y)} q_j^{(\phi_y)} q_h^{(\phi_y)} dx dy \\
& + D_{22} \iint_R p_i^{(\phi_y)} p_k^{(\phi_y)} q_j^{(\phi_y)} q_h^{(\phi_y)} dx dy \\
& + D_{26} \iint_R (p_i^{(\phi_y)} p_k^{(\phi_y)} q_j^{(\phi_y)} q_h^{(\phi_y)} \\
& \quad + p_i^{(\phi_y)} p_k^{(\phi_y)} q_j^{(\phi_y)} q_h^{(\phi_y)}) dx dy \\
& + D_{66} \iint_R p_i^{(\phi_y)} p_k^{(\phi_y)} q_j^{(\phi_y)} q_h^{(\phi_y)} dx dy \\
& + r_1 \int_0^a p_i^{(\phi_y)} p_k^{(\phi_y)} [q_j^{(\phi_y)} q_h^{(\phi_y)}]_{y=0} dx \\
& + r_3 \int_0^a p_i^{(\phi_y)} p_k^{(\phi_y)} [q_j^{(\phi_y)} q_h^{(\phi_y)}]_{y=b} dx.
\end{aligned} \tag{A.2}$$

with $K = 5/6$

$$[\mathbf{M}] = \begin{bmatrix} [M_{ijkh}^{uu}] & 0 & 0 & 0 & 0 \\ & [M_{ijkh}^{vv}] & 0 & 0 & 0 \\ & & [M_{ijkh}^{ww}] & 0 & 0 \\ & & & [M_{ijkh}^{\phi_x\phi_x}] & 0 \\ \text{sym} & & & & [M_{ijkh}^{\phi_y\phi_y}] \end{bmatrix},$$

$$M_{ijkh}^{uu} = I_0 \iint_R p_i^{(u)} p_k^{(u)} q_j^{(u)} q_h^{(u)} dx dy,$$

$$M_{ijkh}^{vv} = I_0 \iint_R p_i^{(v)} p_k^{(v)} q_j^{(v)} q_h^{(v)} dx dy,$$

$$M_{ijkh}^{ww} = I_0 \iint_R p_i^{(w)} p_k^{(w)} q_j^{(w)} q_h^{(w)} dx dy,$$

$$M_{ijkh}^{\phi_x\phi_x} = I_2 \iint_R p_i^{(\phi_x)} p_k^{(\phi_x)} q_j^{(\phi_x)} q_h^{(\phi_x)} dx dy,$$

$$M_{ijkh}^{\phi_y\phi_y} = I_2 \iint_R p_i^{(\phi_y)} p_k^{(\phi_y)} q_j^{(\phi_y)} q_h^{(\phi_y)} dx dy.$$

(A.3)

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